

Electronic Supplementary Materials

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**Dynamic response of bilayered saturated porous media based on
fractional thermoelastic theory**

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Data S1 Derivation of the analytical solution for Eqs. (25) and (26)

For clarity, Eqs. (25) and (26) can be specifically rewritten for medium ① as:

$$\left[\frac{\partial^2}{\partial x^2} - \left(\frac{b_1 i \omega}{(\lambda_1 + 2\mu_1)\xi_2} + \frac{\rho_f \omega^2}{\rho_1} - \omega^2 \right) \right] e_1 = \left[\frac{\beta_1 T_0}{\lambda_1 + 2\mu_1} \frac{\partial^2}{\partial x^2} - \frac{b_1 \alpha_{f1} i \omega T_0}{(\lambda_1 + 2\mu_1)\xi_2} \right] \theta_1, \quad (\text{A-1})$$

$$\frac{\beta_1 i \omega}{m_1} \left(1 + \frac{\tau_1^{\alpha_1} (i\omega)^{\alpha_1}}{\alpha_1!} \right) e_1 = \left[\frac{\partial^2}{\partial x^2} - i\omega \left(1 + \frac{\tau_1^{\alpha_1} (i\omega)^{\alpha_1}}{\alpha_1!} \right) \right] \theta_1, \quad (\text{A-2})$$

Eqs. (A-1) and (A-2) can be further simplified as:

$$\left(\frac{\partial^2}{\partial x^2} - a_1 \right) e_1 = \left(a_4 \frac{\partial^2}{\partial x^2} - a_5 \right) \theta_1, \quad (\text{A-3})$$

$$a_3 e_1 = \left(\frac{\partial^2}{\partial x^2} - a_2 \right) \theta_1, \quad (\text{A-4})$$

where $a_1 = \frac{b_1 i \omega}{(\lambda_1 + 2\mu_1)\xi_2} + \frac{\rho_f \omega^2}{\rho_1} - \omega^2$, $a_2 = i\omega \left(1 + \frac{\tau_1^{\alpha_1} (i\omega)^{\alpha_1}}{\alpha_1!} \right)$, $a_3 = \frac{\beta_1 i \omega}{m_1} \left(1 + \frac{\tau_1^{\alpha_1} (i\omega)^{\alpha_1}}{\alpha_1!} \right)$, $a_4 = \frac{\beta_1 T_0}{\lambda_1 + 2\mu_1}$,

and $a_5 = \frac{b_1 i \omega \alpha_{f1} T_0}{(\lambda_1 + 2\mu_1)\xi_2}$.

Combining Eq. (A-3) and Eq. (A-4), one obtains the following fourth order partial differential equation:

$$\left(\frac{\partial^4}{\partial x^4} - A_1 \frac{\partial^2}{\partial x^2} + A_2 \right) \theta_1 = 0, \quad (\text{A-5})$$

where $A_1 = a_1 + a_2 + a_3 a_4$ and $A_2 = a_1 a_2 + a_3 a_5$.

In a similar manner, the following expression can be derived:

$$\left(\frac{\partial^4}{\partial x^4} - A_1 \frac{\partial^2}{\partial x^2} + A_2 \right) e_1 = 0, \quad (\text{A-6})$$

Eq. (A-5) can be further decomposed to:

$$\left(\frac{\partial^2}{\partial x^2} - M_1^2 \right) \left(\frac{\partial^2}{\partial x^2} - M_2^2 \right) \theta_1 = 0, \quad (\text{A-7})$$

where $M_1^2 = \frac{A_1 + \sqrt{A_1^2 - 4A_2}}{2}$ and $M_2^2 = \frac{A_1 - \sqrt{A_1^2 - 4A_2}}{2}$ are the characteristic roots of Eq. (A-5).

Consequently, the solution of Eq. (A-5) can be given by:

$$\theta_1 = \sum_{i=1}^2 B_i e^{-M_i x} + \sum_{i=1}^2 C_i e^{M_i x}, \quad (\text{A-8})$$

where B_i and C_i are undetermined coefficients.

Data S2 Derivation of the analytical solution for medium 2

And similarly, the governing equations of medium ② are obtained as:

$$\left[\frac{\lambda_2 + 2\mu_2}{\rho_2 \xi_1^2} \frac{\partial^2}{\partial x^2} - \left(\frac{b_2 i \omega}{\rho_2 \xi_1^2 \xi_2} + \frac{\rho_{f2} \omega^2}{\rho_2} - \omega^2 \right) \right] e_2 = \left(\frac{\beta_2 T_0}{\rho_2 \xi_1^2} \frac{\partial^2}{\partial x^2} - \frac{b_2 i \omega \alpha_{f2} T_0}{\rho_2 \xi_1^2 \xi_2} \right) \theta_2, \quad (\text{B-1})$$

$$\frac{\beta_2 i \omega}{k_2 \xi_2} \left(1 + \frac{\tau_2^{\alpha_2} (i\omega)^{\alpha_2}}{\alpha_2!} \right) e_2 = \left[\frac{\partial^2}{\partial x^2} - \frac{m_2 i \omega}{k_2 \xi_2} \left(1 + \frac{\tau_2^{\alpha_2} (i\omega)^{\alpha_2}}{\alpha_2!} \right) \right] \theta_2, \quad (\text{B-2})$$

Eqs. (B-1) and (B-2) can be respectively simplified as:

$$\left(\eta_1 \frac{\partial^2}{\partial x^2} - \eta_2 \right) e_2 = \left(\eta_3 \frac{\partial^2}{\partial x^2} - \eta_4 \right) \theta_2, \quad (\text{B-3})$$

$$\eta_5 e_2 = \left(\frac{\partial^2}{\partial x^2} - \eta_6 \right) \theta_2, \quad (\text{B-4})$$

where $\eta_1 = \frac{\lambda_2 + 2\mu_2}{\rho_2 \xi_1^2}$, $\eta_2 = \frac{b_2 i \omega}{\rho_2 \xi_1^2 \xi_2} + \frac{\rho_{f2} \omega^2}{\rho_2} - \omega^2$, $\eta_3 = \frac{\beta_2 T_0}{\rho_2 \xi_1^2}$, $\eta_4 = \frac{b_2 i \omega \alpha_{f2} T_0}{\rho_2 \xi_1^2 \xi_2}$, $\eta_5 = \frac{\beta_2 i \omega \left(1 + \frac{\tau_2^{\alpha_2} (i\omega)^{\alpha_2}}{\alpha_2!} \right)}{k_2 \xi_2}$,

and $\eta_6 = \frac{m_2 i \omega}{k_2 \xi_2} \left(1 + \frac{\tau_2^{\alpha_2} (i\omega)^{\alpha_2}}{\alpha_2!} \right)$.

Similar to the derivation process of medium ①, a similar equation for medium ② is obtained from Eqs. (B-3) and (B-4) as:

$$\left(\eta_1 \frac{\partial^4}{\partial x^4} - A_3 \frac{\partial^2}{\partial x^2} + A_4 \right) \theta_2 = 0, \quad (\text{B-5})$$

where $A_3 = \eta_1 \eta_6 + \eta_2 + \eta_3 \eta_5$ and $A_4 = \eta_2 \eta_6 + \eta_4 \eta_5$.

In a similar manner, the following expression can be derived:

$$\left(\eta_1 \frac{\partial^4}{\partial x^4} - A_3 \frac{\partial^2}{\partial x^2} + A_4 \right) e_2 = 0, \quad (\text{B-6})$$

Eq. (B-5) can be factorized as:

$$\left(\frac{\partial^2}{\partial x^2} - N_1^2 \right) \left(\frac{\partial^2}{\partial x^2} - N_2^2 \right) \theta_2 = 0, \quad (\text{B-7})$$

where $N_1^2 = \frac{A_3 + \sqrt{A_3^2 - 4\eta_1 A_4}}{2\eta_1}$ and $N_2^2 = \frac{A_3 - \sqrt{A_3^2 - 4\eta_1 A_4}}{2\eta_1}$ are the characteristic roots of Eq. (B-5).

Consequently, according to the boundary conditions $x \rightarrow \infty$, $\theta_2 = 0$, $u_2 = 0$, and $p_{f2} = 0$, the solution of Eq. (B-5) can be given by:

$$\theta_2 = \sum_{i=1}^2 E_i e^{-N_i x}, \quad (\text{B-8})$$

Similarly, the following expressions can be derived:

$$e_1 = \sum_{i=1}^2 G_i e^{-M_i x} + \sum_{i=1}^2 H_i e^{M_i x}, \quad (\text{B-9})$$

$$e_2 = \sum_{i=1}^2 I_i e^{-N_i x}, \quad (\text{B-10})$$

where E_i , G_i , H_i , and I_i are undetermined coefficients.

Substituting Eqs. (A-8) and (B-9) into Eq. (A-4), the relationship between B_i and G_i , as well as that between C_i and H_i can be derived as:

$$G_i = \delta_i B_i, \quad H_i = \delta_i C_i, \quad (\text{B-11})$$

$$\text{where } \delta_i = \frac{M_i^2 - a_2}{a_3}.$$

In addition, substituting Eqs. (B-8) and (B-10) into Eq. (B-3), the relationship between E_i and I_i can be derived:

$$I_i = \gamma_i E_i, \quad (\text{B-12})$$

$$\text{where } \gamma_i = \frac{N_i^2 - \eta_6}{\eta_5}.$$

Therefore, e_1 and e_2 can be respectively expressed as:

$$e_1 = \sum_{i=1}^2 \delta_i B_i e^{-M_i x} + \sum_{i=1}^2 \delta_i C_i e^{M_i x}, \quad (\text{B-13})$$

$$e_2 = \sum_{i=1}^2 \gamma_i E_i e^{-N_i x}, \quad (\text{B-14})$$

According to $e_j = \partial u_j / \partial x$ and the boundary condition given by Eqs. (3)~(5), u_1 and u_2 can be respectively expressed as:

$$u_1 = - \sum_{i=1}^2 \frac{\delta_i}{M_i} B_i e^{-M_i x} + \sum_{i=1}^2 \frac{\delta_i}{M_i} C_i e^{M_i x} + J_1, \quad (\text{B-15})$$

$$u_2 = - \sum_{i=1}^2 \frac{\gamma_i}{N_i} E_i e^{-N_i x}, \quad (\text{B-16})$$

Substituting Eqs. (A-8) and (B-15) into Eq. (20), the pore water pressure in the first layer can be written as:

$$p_{f1} = \sum_{i=1}^2 \left[\frac{\lambda_1 + 2\mu_1}{\mu_1} \delta_i - \frac{\beta_1 T_0}{\mu_1} + \frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} \frac{\delta_i}{M_i^2} \right] B_i e^{-M_i x} + \sum_{i=1}^2 \left[\frac{\lambda_1 + 2\mu_1}{\mu_1} \delta_i - \frac{\beta_1 T_0}{\mu_1} + \frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} \frac{\delta_i}{M_i^2} \right] C_i e^{M_i x} + \frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} J_1 x + J_2, \quad (B-17)$$

where J_1 and J_2 are undetermined coefficients.

Substituting Eqs. (B-8) and (B-16) into Eq. (20), the pore water pressure in the second layer can be written as:

$$p_{f2} = \sum_{i=1}^2 \left[\frac{\lambda_2 + 2\mu_2}{\mu_1} \gamma_i - \frac{\beta_2 T_0}{\mu_1} + \frac{\omega^2 \rho_2 \xi_1^2}{\mu_1} \frac{\gamma_i}{N_i^2} \right] E_i e^{-N_i x}, \quad (B-18)$$

Substituting Eqs. (A-8), (B-15), and (B-16) into Eq. (19), the stresses in the first and second layers can be obtained as:

$$\sigma_1 = - \sum_{i=1}^2 \left[\frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} \frac{\delta_i}{M_i^2} \right] B_i e^{-M_i x} - \sum_{i=1}^2 \left[\frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} \frac{\delta_i}{M_i^2} \right] C_i e^{M_i x} - \frac{\omega^2 (\lambda_1 + 2\mu_1)}{\mu_1} J_1 x - J_2, \quad (B-19)$$

$$\sigma_2 = - \sum_{i=1}^2 \frac{\omega^2 \rho_2 \xi_1^2}{\mu_1} \frac{\gamma_i}{N_i^2} E_i e^{-N_i x}. \quad (B-20)$$

Performing normalization on Eqs. (1), (2), and (6)~(11), the corresponding expressions can be written in frequency domain as follows:

$$\sigma_1|_{x=0} = 0, \quad (B-21)$$

$$\theta_1|_{x=0} = \theta_0, \quad (B-22)$$

$$p_{f1}|_{x=0} = 0, \quad (B-23)$$

$$X_T \frac{\partial \theta_1}{\partial x} \Big|_{x=h} = - \left[1 + \frac{\tau_1^{\alpha_1}}{\alpha_1!} (i\omega)^{\alpha_1} \right] (\theta_1|_{x=h} - \theta_2|_{x=h}). \quad (B-24)$$

where $X_T = k_1 \xi_1^2 \xi_2^2 / hm$ denotes the dimensionless thermal contact resistance.

$$\frac{\partial \theta_1}{\partial x} \Big|_{x=h} = \frac{k_2}{k_1} \frac{\left[1 + \frac{\tau_1^{\alpha_1}}{\alpha_1!} (i\omega)^{\alpha_1} \right]}{\left[1 + \frac{\tau_2^{\alpha_2}}{\alpha_2!} (i\omega)^{\alpha_2} \right]} \frac{\partial \theta_2}{\partial x} \Big|_{x=h}, \quad (B-25)$$

$$u_1|_{x=h} = u_2|_{x=h}, \quad (B-26)$$

$$\frac{\sigma_2|_{x=h}}{\sigma_1|_{x=h}} = \frac{2}{1 + Z_1/Z_2}, \quad (B-27)$$

$$p_{f1}|_{x=h} = p_{f2}|_{x=h}. \quad (B-28)$$

Substituting Eqs. (A-8), (B-8) and (B-15)~(B-20) into Eqs. (B-21)~(B-28), the undetermined coefficients B_i , C_i , E_i , and J_i can be derived, which form the analytical solutions to the THM coupling response of the bilayered saturated porous media.