

## Electronic Supplementary Materials

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# Bogie active stability simulation and scale rig test based on frame lateral vibration control

Ya-dong SONG, Hu LI, Jun CHENG, Yuan YAO

*State Key Laboratory of Traction Power, Southwest Jiaotong University, Chengdu 610031, China*

**Table S1 The scale bogie model parameters**

Symbol	Definition	Value
$m_w$	Mass of the wheelset	14.7 kg
$I_w$	Yaw inertia of the wheelset	0.32 kg m <sup>2</sup>
$m_f$	Mass of bogie frame	14.5 kg
$I_f$	Yaw inertia of bogie frame	3.3 kg m <sup>2</sup>
$m_m$	Mass of actuator	10.9 kg
$k_{px}$	Primary longitudinal stiffness per axle	20 kN/m
$k_{py}$	Primary lateral stiffness per axle	2.0 kN/mm
$k_{sx}$	Secondary longitudinal stiffness	1.3 kN/m
$k_{sy}$	Secondary lateral stiffness	1.3 kN/m
$c_{sx}$	Yaw damper damping	0
$c_{sy}$	Secondary lateral damper damping	2.0 kN s/m
$f_m$	Actuator suspension frequency	0.1 Hz
$\xi_m$	Actuator suspension damping ratio	0.3
$l_m$	Longitudinal distance from actuator suspension to bogie center	0.45 m
$2b$	Wheel base	0.56 m
$2l_0$	Distance of the contact spot	0.2986 m
$2l_1$	Lateral spacing of primary suspension	0.422 m
$2l_2$	Lateral spacing of secondary suspension	0.4 m
$f_\eta$	The lateral creep coefficient	10 kN
$f_\zeta$	The longitudinal creep coefficient	10 kN
$k_{gy}$	The gravitational stiffness	0
$k_{g\psi}$	The gravitational angular stiffness	0
$r_0$	The wheel rolling radius	0.1 m
$\lambda$	Wheel–rail contact conicity	0.1
$v$	Speed	50 km/h

### Data S1 The matrices of the bogie model

$$\begin{aligned}
\mathbf{C} &= \begin{bmatrix} \frac{2f_\eta}{v} \\ \frac{2l_0^2 f_\zeta}{v} \\ \frac{2f_\eta}{v} \\ \frac{2l_o^2 f_\zeta}{v} \\ c_{sy} + 2c_{my} & -c_{my} & -c_{my} \\ l_2^2 c_{sx} + 2l_m^2 c_{my} & -l_m c_{my} & l_m c_{my} \\ -c_{my} & -l_m c_{my} & c_{my} \\ -c_{my} & l_m c_{my} & c_{my} \end{bmatrix} \\
\mathbf{K} &= \begin{bmatrix} k_{py} + k_{gy} & -2f_\eta & -k_{py} & -bk_{py} \\ \frac{2\lambda l_0 f_\zeta}{r_0} & l_1^2 k_{px} + k_{g\psi} & -l_1^2 k_{px} & -l_1^2 k_{px} \\ k_{py} + k_{gy} & -2f_\eta & -k_{py} & bk_{py} \\ \frac{2\lambda l_0 f_\zeta}{r_0} & l_1^2 k_{px} + k_{g\psi} & -l_1^2 k_{px} & -l_1^2 k_{px} \\ -k_{py} & -k_{py} & 2k_{py} + k_{sy} + 2k_{my} & -k_{my} & -k_{my} \\ -bk_{py} & -l_1^2 k_{px} & bk_{py} & -l_1^2 k_{px} & +2b^2 k_{py} + 2l_m^2 k_{my} \\ & & -l_1^2 k_{px} & -k_{my} & -l_m k_{my} \\ & & & -k_{my} & l_m k_{my} \\ & & & & k_{my} \end{bmatrix} \\
\mathbf{M} &= \begin{bmatrix} m_w & & & & \\ & I_w & & & \\ & & m_w & & \\ & & & I_w & \\ & & & & m_f \\ & & & & & I_f \\ & & & & & & m_m \\ & & & & & & & m_m \end{bmatrix} \\
\mathbf{E} &= \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & l_m & 0 & 0 \end{bmatrix}^T \\
\mathbf{Q} &= \begin{bmatrix} k_{py} & 0 & k_{py} & 0 & 0 & 0 & 0 & 0 \end{bmatrix}^T \\
\mathbf{K}_C &= \begin{bmatrix} 0 & 0 & 0 & 0 & k_{d1} & k_{d1} & 0 & 0 & 0 & 0 & 0 & 0 & k_{v1} & k_{v1} & 0 & 0 \\ 0 & 0 & 0 & 0 & k_{d2} & k_{d2} & 0 & 0 & 0 & 0 & 0 & 0 & k_{v2} & k_{v2} & 0 & 0 \end{bmatrix}
\end{aligned}$$