



## Differential coupling contributes to synchronization via a capacitor connection between chaotic circuits<sup>\*</sup>

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**Abstract:** Nonlinear oscillators and circuits can be coupled to reach synchronization and consensus. The occurrence of complete synchronization means that all oscillators can maintain the same amplitude and phase, and it is often detected between identical oscillators. However, phase synchronization means that the coupled oscillators just keep pace in oscillation even though the amplitude of each node could be different. For dimensionless dynamical systems and oscillators, the synchronization approach depends a great deal on the selection of coupling variable and type. For nonlinear circuits, a resistor is often used to bridge the connection between two or more circuits, so voltage coupling can be activated to generate feedback on the coupled circuits. In this paper, capacitor coupling is applied between two Pikovsk-Rabinovich (PR) circuits, and electric field coupling explains the potential mechanism for differential coupling. Then symmetric coupling and cross coupling are activated to detect synchronization stability, separately. It is found that resistor-based voltage coupling via a single variable can stabilize the synchronization, and the energy flow of the controller is decreased when synchronization is realized. Furthermore, by applying appropriate intensity for the coupling capacitor, synchronization is also reached and the energy flow across the coupling capacitor is helpful in regulating the dynamical behaviors of coupled circuits, which are supported by a continuous energy exchange between capacitors and the inductor. It is also confirmed that the realization of synchronization is dependent on the selection of a coupling channel. The approach and stability of complete synchronization depend on symmetric coupling, which is activated between the same variables. Cross coupling between different variables just triggers phase synchronization. The capacitor coupling can avoid energy consumption for the case with resistor coupling, and it can also enhance the energy exchange between two coupled circuits.

**Key words:** Synchronization; Voltage coupling; Chaotic circuit; Capacitor coupling

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### 1 Introduction

Analog circuits can be built to detect and analyze the outputs of many nonlinear dynamical systems (Ikezi et al., 1983; Timmer et al., 2000; Kiliç et al., 2002; Haniyas et al., 2006; Muthuswamy and Chua, 2010), which can generate periodic and chaotic series. For example, neural circuits (Davison and Ehlers,

2011; Adesnik et al., 2012; Ren et al., 2017; Zhang et al., 2018a) can be designed to reproduce the main dynamical properties of electrical activities in an isolated neuron and coupled neurons. The neural network of circuits can be effective in investigating the collective behaviors of a nervous system. Nonlinear analysis provides reliable methodologies for signal processing and decoding of information. The circuit equations can be described when electric devices are connected to build any oscillatory circuit according to Kirchhoff's law. Furthermore, scale transformation is applied to obtain dimensionless dynamical systems, so a reliable algorithm can be used to find numerical solutions for the variables, and

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then feasible procedures (Andrievskii and Fradkov, 2004; Nazzal and Natsheh, 2007; Schöll and Schuster, 2008; Wang et al., 2012, 2015; Guo et al., 2018) can be activated for target control.

Synchronization can be triggered when an appropriate coupling is applied between two or more agents, and it is thought of as a class of cooperation and competition via exchange of energy flow. For multi-agent systems and a network of oscillators, internal cooperation and external forcing (periodic or even noise) (Qin et al., 2014; Ma et al., 2015) can enhance the realization of consensus in dynamical behaviors such as amplitude and phase. An isolated circuit generates a finite signal in amplitude and even chaotic circuits can generate a variety of signals with frequency differences. Nonlinear circuits can be coupled to enhance the power of outputs, and synchronization based on chaotic circuits has potential applications in secure communications (Wu and Chua, 1993; Boccaletti et al., 1997; Zaher and Abu-Rezq, 2011). Some researchers regard the nervous system as a complex network of integrated circuits, and each neuron is thought of as an effective nonlinear circuit for signal processing. Electric synapses and chemical synapses (Eccles, 1982; Bennett, 1997, 2000; Kopell and Ermentrout, 2004; Song et al., 2015) play important roles in receiving and propagating signals. Gap junction coupling (Bennett, 1997; Song et al., 2015) is often used to investigate the electrical response between neurons connected with electric synapses, and even most biological researchers argue that neurons should be considered as a chemical synapse connection. Indeed, a gap junction is the same as voltage coupling via a resistor, which can consume certain energy during signal processing and propagation. As a result, the power consumption of coupling resistors can be very large when millions of neurons are connected via complex paths or links. Chemical synapse coupling (Balenzuela and García-Ojalvo, 2005; Li et al., 2007; Burić et al., 2008) depends on the diffusion of neurotransmitters, and the cost of Joule heat on the coupling resistor is removed; therefore, it provides important guidance for circuit synchronization.

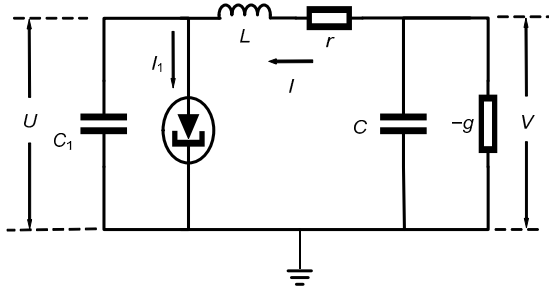
It is well known that a resistor connection just generates voltage coupling and the difference between output voltages from the nonlinear circuits bridged by a resistor can induce time-varying feed-

back on each circuit by applying an external stimulus. Indeed, when a capacitor is used to bridge a connection between two nonlinear circuits, the outputs from each circuit can charge the plates, and the distribution of electric field in the capacitor will be changed. As a result, the exchange of field energy and charges will impose appropriate feedback on both of the coupled circuits. In this paper, two Pikovsk-Rabinovich (PR) chaotic circuits (Pikovsky and Rabinovich, 1978) are connected with a resistor and capacitor to detect when synchronization is realized for each. Symmetric coupling in the same channel and cross coupling between different channels are used to investigate the stability of synchronization.

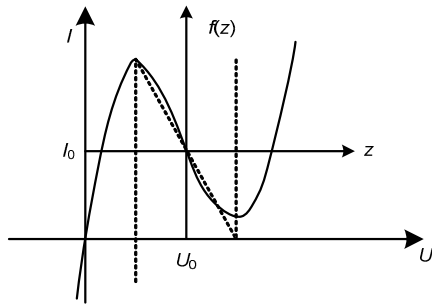
## 2 Model description and method

Nonlinear electric devices are critical for building chaotic circuits. The well-known nonlinear electric devices include the negative resistor, nonlinear capacitor, nonlinear inductor, and memristor (Muthuswamy and Kokate, 2009; Buscarino et al., 2012; Budhathoki et al., 2013; Bao et al., 2016, 2017; Zhang et al., 2018b). A negative resistor  $R$  requires the nonlinear dependence of voltage on current. A nonlinear capacitor means that the charges  $q$  on the plates change the voltage of the capacitor in a nonlinear relation. In sum, the main characteristic of nonlinear devices is that the change in an output variable does not follow the change in the input variable proportionally. These nonlinear electric devices can be applied to build a variety of chaotic circuits, and robust synchronization (Buscarino et al., 2009) can be further investigated between hyperchaotic circuits through experiments. For example, an autonomous and self-excited circuit (Pikovsky and Rabinovich, 1978; Pikovsky, 1981; He et al., 2003; Louodop et al., 2014) was built by Pikovsk and Rabinovich in 1978. The circuit was made of a capacitor  $C$ , a linear resistor  $r$ , an inductor  $L$ , a nonlinear resistor with negative conductance  $-g$ , and a tunnel diode with parasitic capacitance  $C_1$ . The circuit is illustrated in Fig. 1.

The tunneling diode can be switched on at a reverse bias and its reverse breakdown voltage is zero, while the quantum tunneling effect can generate a region of negative resistance under a forward bias. Fig. 2 shows the voltage-current ( $U$ - $I$ ) curve of this tunneling diode.



**Fig. 1** Schematic of a Pikovsk-Rabinovich (PR) circuit, a self-excited oscillator



**Fig. 2**  $I$ - $U$  characteristic of the tunnel diode

The output voltage for capacitor  $C_1$  is denoted as  $U$ , while  $V$  represents the voltage for negative conductance.  $I$  is the current across inductor  $L$ , and  $I_1$  describes the current across the tunnel diode,  $I_1 = I_0 + I_0[(U/U_0 - 1)^3 - (U/U_0 - 1)]$

According to the physical Kirchhoff law, the circuit equations for Fig. 1 can be approached as

$$\begin{cases} V - U = rI + L \frac{dI}{dt}, \\ -I = C \frac{dV}{dt} - gV, \\ I = I_1 + C_1 \frac{dU}{dt}. \end{cases} \quad (1)$$

For further dynamical analysis and numerical studies, scale transformation is proposed to obtain a dimensionless dynamical system. It requires the variable transformation as follows:

$$\begin{cases} x = \frac{I}{I_0} - 1, y = \frac{V - Ir - U_0}{\omega LI_0}, z = \frac{U}{U_0} - 1, \tau = t\omega, \\ \omega = \sqrt{\frac{1 - gr}{LC}}, \delta = \frac{U_0}{\omega LI_0}, 2\gamma = \frac{gL - rC}{\omega LC}, \\ \alpha = \frac{rU_0}{\omega^2 L^2 I_0}, \beta = -1 + \frac{gU_0}{\omega^2 I_0 LC}, \mu = \frac{I_0}{\omega C_1 U_0}. \end{cases} \quad (2)$$

As a result, the dimensionless dynamical system can be described by three-variable ordinary differential equations (ODEs) as follows:

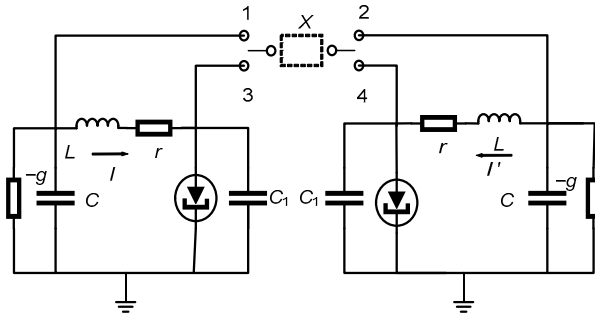
$$\begin{cases} \frac{dx}{d\tau} = y - \delta z, \\ \frac{dy}{d\tau} = -x + 2\gamma y + \alpha z + \beta, \\ \frac{dz}{d\tau} = \mu(x + z - z^3). \end{cases} \quad (3)$$

The dynamics (3) can be investigated via bifurcation analysis, and different attractors can be formed by setting appropriate parameters. For example, a chaotic series can be observed by applying the parameters as  $\delta=0.66$ ,  $\gamma=0.201$ ,  $\alpha=0.165$ ,  $\beta=0$ , and  $\mu=1/0.047$ . From a control view, the stabilization of variable  $y$  is very important for control of chaos. In the case of synchronization problems, two identical PR circuits are often coupled via different channels or variables. The coupled circuits are plotted in Fig. 3, where  $X$  describes the coupling channel; for example, when the output ends 1-2 or 3-4 are connected, symmetric coupling is activated so that the same variables are coupled. However, cross coupling is switched on when the output ends 1-4 or 3-2 are connected so that different variables are coupled. The coupled PR circuits under bidirectional coupling can be described by

$$\begin{cases} L \frac{dI}{dt} = V - U - rI, \\ C \frac{dV}{dt} = gV - I - \lambda_1 I_X, \\ C_1 \frac{dU}{dt} = I - I_1 - \lambda_3 I_X, \end{cases} \quad \begin{cases} L \frac{d\hat{I}}{dt} = \hat{V} - \hat{U} - r\hat{I}, \\ C \frac{d\hat{V}}{dt} = g\hat{V} - \hat{I} + \lambda_2 I_X, \\ C_1 \frac{d\hat{U}}{dt} = \hat{I} - \hat{I}_1 + \lambda_4 I_X, \end{cases} \quad (4)$$

where parameters  $\lambda_1$ ,  $\lambda_2$ ,  $\lambda_3$ , and  $\lambda_4$  decide the on-off state for the coupling device by resetting 0 and 1. Resistor-based voltage coupling and capacitor-based current (for an electric field) coupling can be defined by

$$I_X = \begin{cases} I_g = \pm g_X (V_i - V_j), \\ I_C = \pm C_X \frac{d(V_i - V_j)}{dt}, \end{cases} \quad (5)$$



**Fig. 3 Schematic of two PR circuits under different coupling channels and styles**

$X$  denotes the coupling devices, which can be resistors or capacitors.  $i=1, 3, j=2, 4$  represent the output ends

where  $g_X$  and  $C_X$  represent the conductance of the coupling resistor and the capacitance of the coupling capacitor, respectively. The variables  $V_i$  and  $V_j$  describe the output voltage from the two PR circuits. The symbol  $\pm$  selects the direction of the coupling current. The coupling current across the coupling device can trigger different forms when different output ends are connected. For the most part, we discuss the effect of resistor coupling and capacitor coupling as well when symmetric and cross coupling are considered, respectively. When the output ends 1, 2 are connected ( $\lambda_1=\lambda_2=1, \lambda_3=\lambda_4=0$ ), the variables  $y, \hat{y}$  are coupled, and the dynamical equations can be described by

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta \\ \quad - \left[ k_1(y - \hat{y}) + k_1 \frac{\alpha}{\delta}(x - \hat{x}) \right], \\ \dot{z} = \mu(x + z - z^3), \\ \dot{\hat{x}} = \hat{y} - \delta \hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta \\ \quad + \left[ k_1(y - \hat{y}) + k_1 \frac{\alpha}{\delta}(x - \hat{x}) \right], \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3), \end{cases} \quad (6)$$

where the coupling coefficient  $k_1 = g_X L^{1/2} / (C - Cgr)^{1/2}$ , and the intrinsic parameters also modulate the coupling intensity. When the output ends 3, 4 are connected ( $\lambda_1=\lambda_2=0, \lambda_3=\lambda_4=1$ ), the dynamical equations for the two coupled systems via resistor coupling can be described by

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta, \\ \dot{z} = \mu[x + z - z^3 - k_2(z - \hat{z})], \\ \dot{\hat{x}} = \hat{y} - \delta \hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta, \\ \dot{\hat{z}} = \mu[\hat{x} + \hat{z} - \hat{z}^3 + k_2(z - \hat{z})], \end{cases} \quad (7)$$

where the coupling coefficient  $k_2 = g_X U_0 / I_0$ , and the intrinsic parameters in the tunnel diode also give possible modulation on the coupling intensity. Eqs. (6) and (7) suggest the case for symmetric coupling. The case for cross coupling is also attractive. When the output ends 3, 2 are connected ( $\lambda_3=\lambda_2=1, \lambda_1=\lambda_4=0$ ), the dynamical equations are given as follows:

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta, \\ \dot{z} = \mu \left[ x + z - z^3 \right. \\ \quad \left. - \left( k_3 z - \frac{k_3}{\delta} \hat{y} - k_3 \frac{\alpha}{\delta^2} \hat{x} - k_3 \frac{\alpha}{\delta^2} \right) \right], \\ \dot{\hat{x}} = \hat{y} - \delta \hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta \\ \quad + \left( k_3 z - \frac{k_3}{\delta} \hat{y} - k_3 \frac{\alpha}{\delta^2} \hat{x} - k_3 \frac{\alpha}{\delta^2} \right), \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3), \end{cases} \quad (8)$$

where the coupling coefficient  $k_3 = g_X U_0 / I_0$ , and the coupling coefficients  $k_1, k_2, k_3$  are approached under  $gr \ll 1$ . That is, cross coupling can be activated by connecting the output ends 3, 2 or 1, 4. For a synchronization stability approach, the error function for the coupled systems can be estimated by

$$\begin{aligned} \theta(e_x, e_y, e_z) &= \sqrt{(x - \hat{x})^2 + (y - \hat{y})^2 + (z - \hat{z})^2} \\ &= \sqrt{e_x^2 + e_y^2 + e_z^2}. \end{aligned} \quad (9)$$

Complete synchronization is stabilized when the error function decreases to zero within a finite transient period, which is dependent on the selection of the coupling coefficient and intensity as well. It is important to discuss the case in which a capacitor

coupling is activated, and then symmetric coupling and cross coupling are investigated, respectively. When the coupling capacitor is switched on between the output ends 1, 2 ( $\lambda_1=\lambda_2=1, \lambda_3=\lambda_4=0$ ), the dynamical equations are confirmed as follows:

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = \frac{k_4}{1+2k_4} \left[ -\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta \right. \\ \quad \left. + \frac{k_4\alpha}{\delta} (y - \hat{y}) + k_4\alpha(\hat{z} - z) \right] \\ \quad + \frac{1+k_4}{1+2k_4} \left[ -x + 2\gamma y + \alpha z + \beta \right. \\ \quad \left. + \frac{k_4\alpha}{\delta} (\hat{y} - y) + k_4\alpha(z - \hat{z}) \right], \\ \dot{z} = \mu(x + z - z^3), \\ \dot{\hat{x}} = \hat{y} - \delta\hat{z}, \\ \dot{\hat{y}} = \frac{k_4}{1+2k_4} \left[ -x + 2\gamma y + \alpha z + \beta \right. \\ \quad \left. + \frac{k_4\alpha}{\delta} (\hat{y} - y) + k_4\alpha(z - \hat{z}) \right] \\ \quad + \frac{1+k_4}{1+2k_4} \left[ -\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta \right. \\ \quad \left. + \frac{k_4\alpha}{\delta} (y - \hat{y}) + k_4\alpha(\hat{z} - z) \right], \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3), \end{cases} \quad (10)$$

where the coupling coefficient  $k_4=C_X/C$ . In fact, as shown in Eq. (5), the capacitor coupling just introduces a differential modulation, and then Eq. (10) is rewritten as Eq. (11).

From the equivalent definition shown in Eq. (11), it is found that the differential error for output voltage is fed back into the coupled circuits with the gain as  $k_4/(2k_4+1)$ , and the additive feedback from variable errors is also triggered when capacitor coupling is switched on. In practice, coupling coefficient  $k_4$  and capacitance  $C_X$  can be tamed to modulate the collective responses of the coupled circuits, and then an appropriate coupling intensity could be effective in realizing synchronization. Furthermore, symmetrical coupling via a capacitor connection is considered between output ends 3, 4 ( $\lambda_1=\lambda_2=0, \lambda_3=\lambda_4=1$ ), and the dynamical equations are achieved as Eq. (12).

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta \\ \quad + \frac{k_4}{1+2k_4} [(-\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta) \\ \quad - (-x + 2\gamma y + \alpha z + \beta)] \\ \quad + \frac{k_4}{1+2k_4} \left[ \frac{\alpha}{\delta} (\hat{y} - y) + \alpha(z - \hat{z}) \right], \\ \dot{z} = \mu(x + z - z^3), \\ \dot{\hat{x}} = \hat{y} - \delta\hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta \\ \quad + \frac{k_4}{1+2k_4} [(-x + 2\gamma y + \alpha z + \beta) \\ \quad - (-\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta)] \\ \quad + \frac{k_4}{1+2k_4} \left[ \frac{\alpha}{\delta} (y - \hat{y}) + \alpha(\hat{z} - z) \right], \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3). \end{cases} \quad (11)$$

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta, \\ \dot{z} = \mu \left[ \frac{1+k_5}{1+2k_5} (x + z - z^3) + \frac{k_5}{1+2k_5} (\hat{x} + \hat{z} - \hat{z}^3) \right], \\ \dot{\hat{x}} = \hat{y} - \delta\hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma\hat{y} + \alpha\hat{z} + \beta, \\ \dot{\hat{z}} = \mu \left[ \frac{1+k_5}{1+2k_5} (\hat{x} + \hat{z} - \hat{z}^3) + \frac{k_5}{1+2k_5} (x + z - z^3) \right]. \end{cases} \quad (12)$$

In Eq. (12) the coupling coefficient  $k_5=C_X/C_1$ . Then Eq. (12) is rewritten with an equivalent form and the differential coupling feedback can be discerned. It reads as Eq. (13) (see the next page).

It is found that differential coupling via a capacitor can be fed back into the coupled circuits under an adjustable gain  $k_5/(1+2k_5)$ , and the synchronization orbits can be tamed to keep them close by applying appropriate coupling gains. Furthermore, when cross coupling via the capacitor is connected between output ends 3, 2 ( $\lambda_3=\lambda_2=1, \lambda_1=\lambda_4=0$ ), it is the same case for a connection between output ends 1, 4 ( $\lambda_3=\lambda_2=0, \lambda_1=\lambda_4=1$ ), and the dynamical equations can be confirmed as Eq. (14).

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta, \\ \dot{z} = \mu(x + z - z^3) \\ \quad + \frac{k_5}{1+2k_5} [\mu(\hat{x} + \hat{z} - \hat{z}^3) - \mu(x + z - z^3)], \\ \dot{\hat{x}} = \hat{y} - \delta \hat{z}, \\ \dot{\hat{y}} = -\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta, \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3) \\ \quad + \frac{k_5}{1+2k_5} [\mu(x + z - z^3) - \mu(\hat{x} + \hat{z} - \hat{z}^3)]. \end{cases} \quad (13)$$

$$\begin{cases} \dot{x} = y - \delta z, \\ \dot{y} = -x + 2\gamma y + \alpha z + \beta, \\ \dot{z} = \frac{k_6 + 0.1}{k_6 + 1.1} \mu(x + z - z^3) \\ \quad + \frac{1}{k_6 + 1.1} \frac{\alpha}{\delta^2} \hat{y} - \frac{1}{k_6 + 1.1} \frac{\alpha}{\delta} \hat{z} \\ \quad + \frac{1}{k_6 + 1.1} \frac{1}{\delta} (-\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta), \\ \dot{\hat{x}} = \hat{y} - \delta \hat{z}, \\ \dot{\hat{y}} = \frac{k_6 + 1}{k_6 + 1.1} (-\hat{x} + 2\gamma \hat{y} + \alpha \hat{z} + \beta) \\ \quad - \frac{0.1}{k_6 + 1.1} \frac{\alpha}{\delta} \hat{y} + \frac{0.1}{k_6 + 1.1} \alpha \hat{z} \\ \quad + \frac{0.1}{k_6 + 1.1} \delta \mu(x + z - z^3), \\ \dot{\hat{z}} = \mu(\hat{x} + \hat{z} - \hat{z}^3). \end{cases} \quad (14)$$

In Eq. (14) the coupling coefficient  $k_6 = C_1/C_X$ , and for simplicity, we set  $C_1/C = 0.1$ . In the same way, coupling gain can be adjusted to find the synchronization orbits. According to our prior knowledge, bi-directional coupling supports complete synchronization between identical oscillators or systems, while phase synchronization (Parlitz et al., 1996; Neiman et al., 1999; Pikovsky et al., 2000; Fell and Axmacher, 2011; Ma et al., 2017) occurs between non-identical systems under coupling. On the other hand, sub-threshold coupling (or weak coupling) can induce phase synchronization between identical systems. The phase series can be detected by applying the Hilbert transform (Hahn, 1996) on the sampled time series for observable variables. Furthermore, the

phase error can be calculated to detect the stability of phase synchronization.

$$\begin{cases} \Delta\phi(t) = \phi(t) - \hat{\phi}(t), \\ \phi(t) = \arctan \frac{\tilde{x}(t)}{x(t)}, \quad \phi'(t) = \arctan \frac{\tilde{\hat{x}}(t)}{\hat{x}(t)}, \\ \tilde{x}(t) = -\frac{1}{\pi} \text{PV} \int_{-\infty}^{\infty} \frac{x(\tau)}{t-\tau} dt, \\ \tilde{\hat{x}}(t) = -\frac{1}{\pi} \text{PV} \int_{-\infty}^{\infty} \frac{\hat{x}(\tau)}{t-\tau} dt, \end{cases} \quad (15)$$

where PV represents the principal value of the integral, and  $\phi(t)$  and  $\phi'(t)$  are the phase series calculated from the time series for outputs  $x(t)$  and  $\hat{x}(t)$ , respectively.

### 3 Numerical results and discussion

In this section, Matlab (ODE45) is applied to find solutions for the dynamical systems under voltage coupling and also under field coupling. The initial values for an isolated PR circuit system are selected as (0.1, 0.1, 0.1), the time step is  $h=0.01$ , the parameters are selected in the chaotic region as  $\delta=0.66$ ,  $\gamma=0.201$ ,  $\alpha=0.165$ ,  $\beta=0$ ,  $\mu=1/0.047$ , and the strange attractor developed is plotted in Fig. 4.

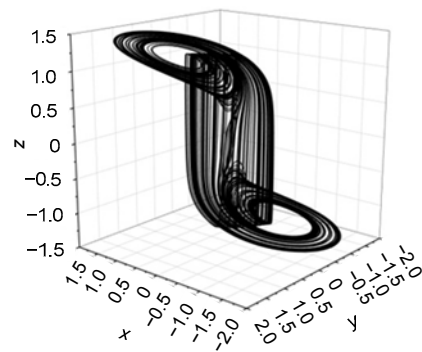
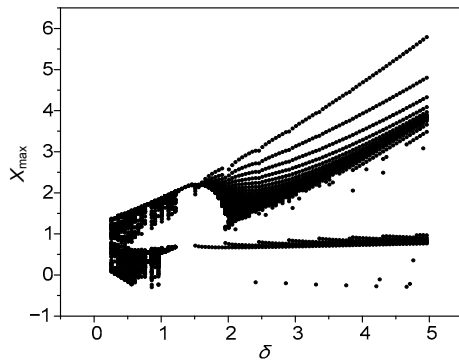


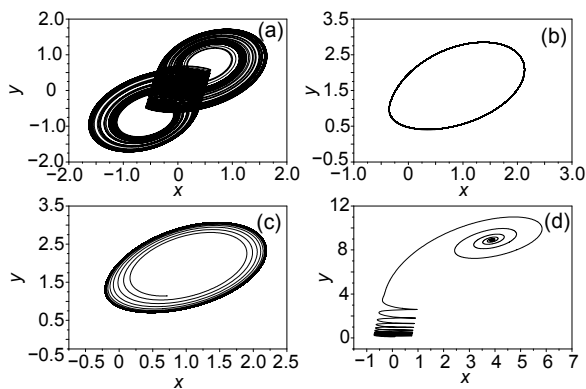
Fig. 4 Formation of a chaotic attractor in a PR circuit

The Lyapunov exponent spectrum can be calculated to find the dependence of chaos occurrence on the parameter setting. For simplicity, the maximum value of the sampled time series for variable  $x$  is estimated and the bifurcation analysis is plotted in Fig. 5.



**Fig. 5** Bifurcation diagram of the maximum value of variable  $x$  vs. parameter  $\delta$  in the PR system

It is shown that chaos can be triggered in a large parameter region. Furthermore, some phase portraits are plotted to illustrate the dependence of the attractor profile on the parameter setting  $\delta$ . The results are shown in Fig. 6.

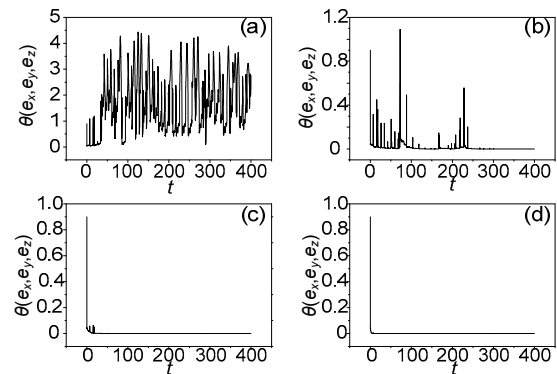


**Fig. 6** Formation of attractors under different parameter values: (a)  $\delta=0.66$ ; (b)  $\delta=1.35$ ; (c)  $\delta=1.5$ ; (d)  $\delta=5$

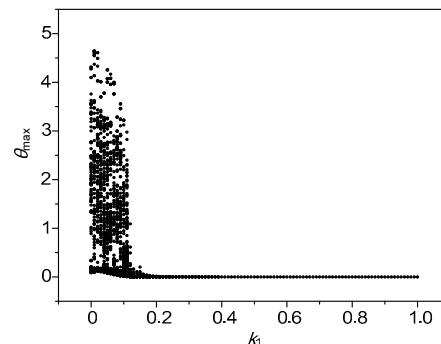
In the following studies, we discuss mainly the synchronization approach and stability between chaotic PR systems. The initial values for the coupled system are selected as (0.1, 0.1, 0.1, 0.1, 0.1, 1), with the same time step of 0.01 applied. First, we investigate the case shown in Eq. (6), by which the output ends 1, 2 are connected via a resistor with conductance  $g_x$ , and the error function is estimated in Fig. 7.

It is confirmed that the error function can decrease to zero within a finite transient period; e.g., it takes about 270 time units when the coupling coefficient is selected as  $k_1=0.12$ . Furthermore, with the increase of coupling intensity, the transient period for

the synchronization approach becomes shorter. Then the dependence of the maximum value of the error function is calculated under different coupling coefficients. The results are shown in Fig. 8.



**Fig. 7** Evolution of the error function via resistor coupling under the connection output ends 1, 2 for  $k_1=0$  (a),  $k_1=0.12$  (b),  $k_1=0.25$  (c), and  $k_1=3.0$  (d)

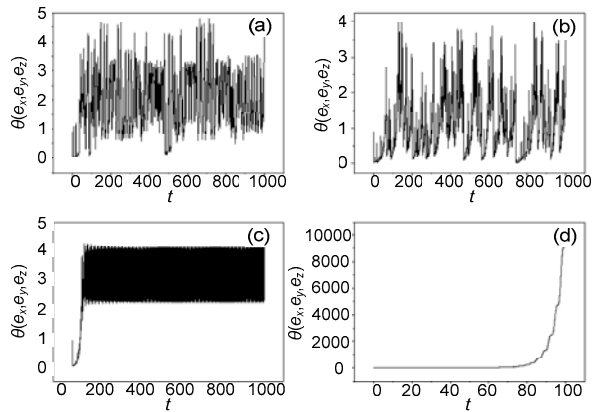


**Fig. 8** Dependence of the maximum error on the coupling coefficient via resistor coupling under connection output ends 1, 2

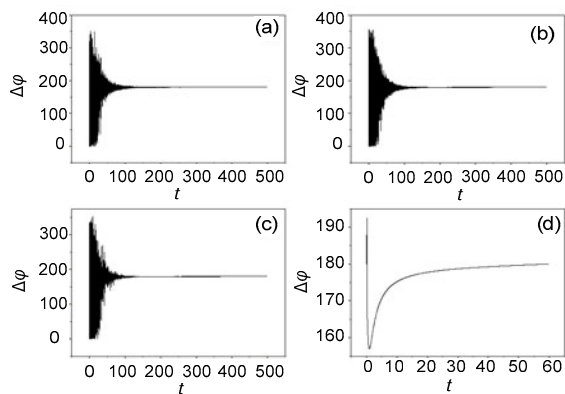
It is shown that the maximum value of the error function can decrease to a finitely small value and that the means toward complete synchronization becomes available via resistor coupling when a single variable is used to couple the chaotic PR systems. Furthermore, the synchronization approach is detected when output ends 3, 4 are connected, for which the dynamical system under resistor coupling is defined in Eq. (7), and the results are plotted in Fig. 9.

Thus, when a coupling resistor is connected between output ends 3, 4, this complete synchronization approach becomes difficult even when the coupling coefficient is further increased. Then, we calculate the evolution of the phase series, which are

calculated using a Hilbert transform as shown in Eq. (15). The results are presented in Fig. 10.



**Fig. 9** Evolution of the error function via resistor coupling under connection output ends 3, 4 for  $k_2=0$  (a),  $k_2=0.3$  (b),  $k_2=0.6$  (c), and  $k_2=1$  (d)

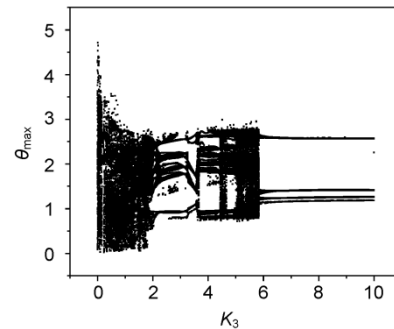


**Fig. 10** Error evolution of a phase series via resistor coupling with a connection between output ends 3, 4 for  $k_2=0$  (a),  $k_2=0.3$  (b),  $k_2=0.5$  (c), and  $k_2=1$  (d)

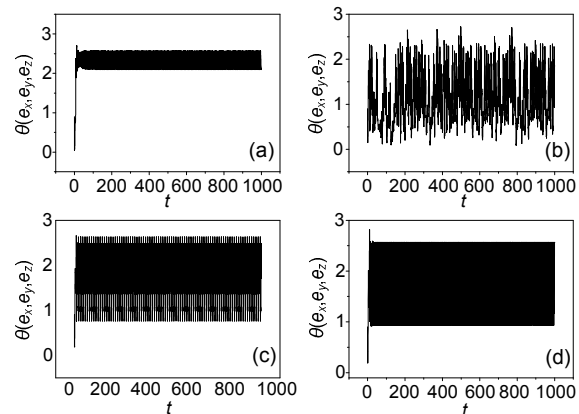
From Fig. 10, it can be seen that anti-phase synchronization can be reached by applying an appropriate coupling coefficient when output ends 3, 4 are connected using resistor coupling. The failure of complete synchronization could be due to the fact that the coupling between the outputs from the tunnel diodes can be suppressed by the outputs from parasitic capacitance  $C_1$  paralleled with the diode. Then, cross coupling is considered between output ends 3, 2, and the dynamical system is described by Eq. (8). The results are plotted in Fig. 11.

With the increase of the coupling coefficient for resistor connection, the maximum value for the error

function just fluctuates between several finite values, and the realization of complete synchronization becomes difficult when a coupling resistor is used to bridge the connection between output ends 3, 2. Consider a clear illustration, where the evolution of the error function is calculated under different coupling coefficients, as shown in Fig. 12.



**Fig. 11** Dependence of the maximum error on the coupling coefficient via resistor coupling with a connection of output ends 3, 2



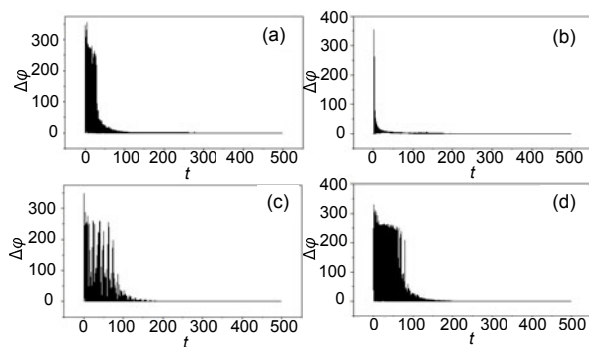
**Fig. 12** Evolution of the error function via resistor coupling under connection output ends 3, 2 for  $k_3=0.2$  (a),  $k_3=1.5$  (b),  $k_3=3.5$  (c), and  $k_3=8$  (d)

The results in Fig. 12 provide evidence that cross coupling via a resistor can generate the coexistence of chaos and periodicity, and the transition from chaos to periodicity can be induced with the increase of the coupling coefficient. Furthermore, we calculate the phase series to observe the occurrence of phase synchronization, and the results are plotted in Fig. 13.

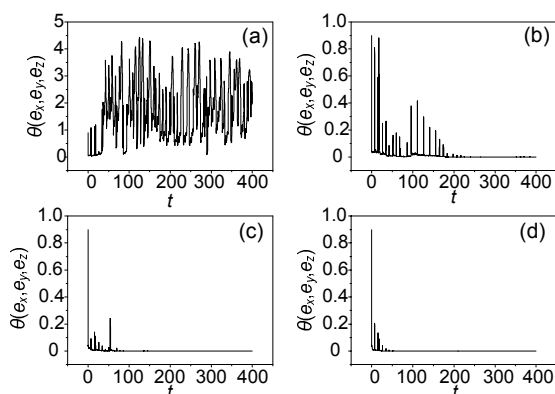
Phase synchronization can be stabilized under cross coupling when the coupling resistor bridges the connection between output ends 3, 2, and the transient



period is shortened with an increase in the coupling coefficient. As mentioned above, capacitor coupling can contribute to the transmission of energy flow between the coupled circuits. Therefore, it is important to discuss the case for capacitor coupling, as mentioned above, where the coupling capacitor is bridged to connect output ends 1, 2 and then symmetric coupling is activated. This case is described by the dynamical system as defined in Eq. (10), and the results are plotted in Fig. 14.



**Fig. 13** Evolution of the phase error under cross coupling via a linear resistor when output ends 3, 2 are connected for  $k_3=0.16$  (a),  $k_3=0.21$  (b),  $k_3=3.2$  (c), and  $k_3=5$  (d)

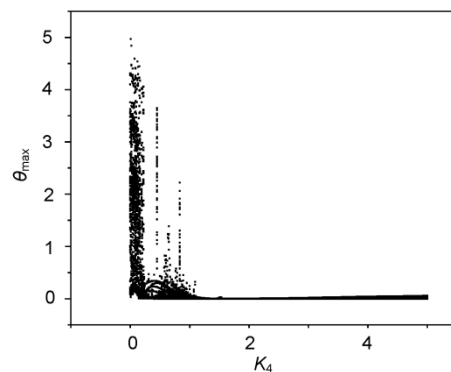


**Fig. 14** Evolution of the error function via capacitor coupling under connection output ends 1, 2 for  $k_4=0$  (a),  $k_4=0.23$  (b),  $k_4=1.0$  (c), and  $k_4=4.0$  (d)

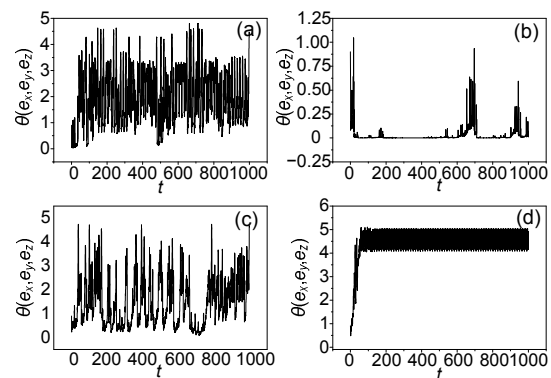
It is verified that complete synchronization between the two chaotic PR systems becomes stable when the coupling capacitor activates symmetrical coupling at the appropriate coupling coefficient, and the transient period becomes shorter with the increase of the coupling coefficient. In addition, the maximum value for the error function is estimated under different coupling coefficients, and the results are illus-

trated in Fig. 15.

The bifurcation diagram predicts that complete synchronization can be reached when capacitor coupling is applied with an appropriate coupling coefficient beyond the threshold of  $k_4 \sim 0.23$ . Capacitor coupling is also considered between output ends 3, 4, whose dynamical system is described by Eq. (12). The results are given in Fig. 16.



**Fig. 15** Dependence of the maximum error on the coupling coefficient via capacitor coupling under connection output ends 1, 2



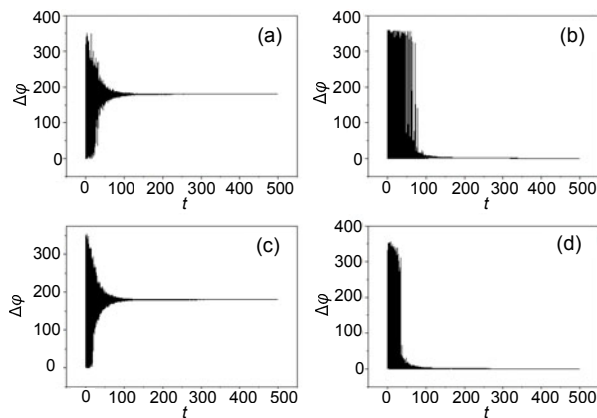
**Fig. 16** Evolution of the error function via capacitor coupling under connection output ends 3, 4 for  $k_5=0$  (a),  $k_5=1$  (b),  $k_5=5$  (c), and  $k_5=11$  (d)

That is to say, complete synchronization between the two chaotic PR systems becomes difficult even if a capacitor is applied to connect output ends 3, 4. Furthermore, the phase series from the two PR systems are calculated to find the possibility of phase synchronization. The results are shown in Fig. 17.

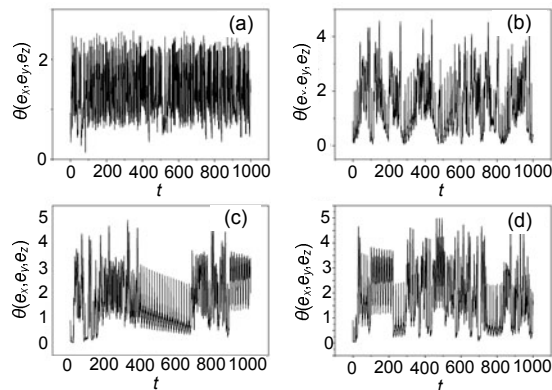
It is found that the two chaotic PR systems can be stabilized at phase synchronization, while anti-phase synchronization is reached with a further

increase of the coupling coefficient for the coupling capacitor. It seems that capacitor coupling shows more efficiency in keeping the stability of phase synchronization and anti-phase synchronization than resistor coupling between output ends 3, 4. Finally, cross coupling via the capacitor is verified by connecting output ends 3, 2, whose dynamical system is described by Eq. (14). The results are shown in Figs. 18 and 19.

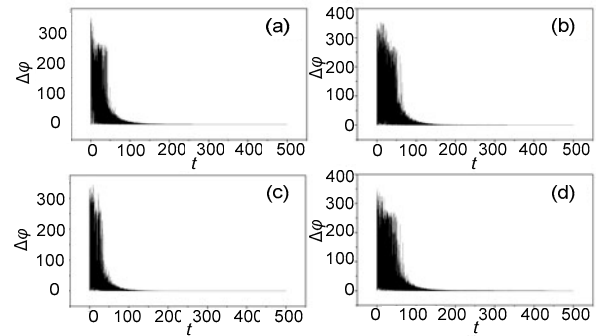
The error function between the two chaotic PR systems becomes time-varying even when the coupling coefficient for the coupling capacitor increases greatly, and extensive numerical results confirm that the profile of chaotic attractors shows distinct diversity and difference. Then the phase series are calculated to analyze the phase synchronization, and the results are plotted in Fig. 19.



**Fig. 17** Evolution of the phase error under cross coupling via a linear resistor when output ends 3, 4 are connected for  $k_5=0$  (a),  $k_5=1$  (b),  $k_5=5$  (c), and  $k_5=7.1$  (d)



**Fig. 18** Evolution of the error function via capacitor coupling under connection output ends 3, 2 for  $k_6=0.01$  (a),  $k_6=0.6$  (b),  $k_6=4$  (c), and  $k_6=10$  (d)



**Fig. 19** Evolution of the phase error under cross coupling via a capacitor when output ends 3, 2 are connected for  $k_6=0.01$  (a),  $k_6=0.6$  (b),  $k_6=4$  (c), and  $k_6=10$  (d)

According to the previous definition for a coupling coefficient, we have  $k_5=1/k_6=C_X/C_1$ ; as a result, the modulation and feedback from the coupling capacitor is enhanced when the coupling capacitor is endowed with a larger value and the synchronization approach becomes relaxed. When the coupling capacitor is selected with finite capacitance values, a certain transient period is needed to reach synchronization stability.

In summary, the synchronization approach depends heavily on the coupling channel and coupling type. The capacitor coupling plays the same role in realizing complete synchronization between chaotic systems, and the coupling capacitor just enhances the energy exchange of the electric field and never consumes energy while the coupling resistor has to consume a certain amount of Joule heat and energy when the coupling is activated. Complete synchronization is realized when resistor coupling or capacitor coupling is applied to connect the outputs from capacitor  $C$  in each circuit, while coupling between parasitic capacitance  $C_1$  in the chaotic PR circuits cannot support complete synchronization other than phase synchronization. Cross coupling via a linear resistor or capacitor can induce phase synchronization. Indeed, a time-varying electric field is induced in the coupling capacitor, and energy flow is transmitted across this coupling capacitor when the coupling connection is switched on. As a result, the coupled circuits are regulated to keep pace with each other, while resistor-based voltage coupling just consumes the Joule energy to suppress nonlinear oscillations in the coupled PR circuits. This type of coupling via capacitor simply provides evidence for understanding

the well-known differential coupling control. On the other hand, a capacitor coupling builds a bridge for the exchange of field energy. For  $L$ - $C$  (inductor and capacitor) circuits, the electric field energy is included in the capacitor while the magnetic field energy stays in the inductor. Then the field energy in the driving, response system and coupling capacitor can be described by

$$\begin{cases} H_1 = \frac{1}{2}CV^2 + \frac{1}{2}C_1U^2 + \frac{1}{2}LI^2, \\ H_2 = \frac{1}{2}C\hat{V}^2 + \frac{1}{2}C_1\hat{U}^2 + \frac{1}{2}L\hat{I}^2, \\ H_{C_x} = \frac{1}{2}C_x(V - \hat{V})^2, \text{ output ends 1, 2 are connected,} \\ H_{C_x} = \frac{1}{2}C_x(U - \hat{U})^2, \text{ output ends 3, 4 are connected.} \end{cases} \quad (16)$$

As a result, the energy storage in the coupling capacitor will decrease to zero when two chaotic PR circuits are synchronized completely. In fact, the field energy flow can be kept in the coupling capacitor, and the capacitance  $C_x$  dominates the transport capacity of energy released from the two coupled PR circuits. Therefore, a continuous exchange of field energy can regulate the dynamics of coupled systems effectively. Because of the conservation of energy, the field energy in the coupling capacitor comes from the energy release as  $H_{C_x} = H_1 - H_2$  in the absence of electromagnetic radiation from these electric devices. The numerical results can be further described to observe the evolution and transport of energy between the coupled systems.

Readers can also extend this study by applying an inductor (induction coil) and memristor between chaotic and hyperchaotic circuits, and interesting results could be confirmed in the forthcoming studies. On the other hand, capacitor coupling just provides insights into field coupling (Guo et al., 2017; Lv et al., 2018; Xu et al., 2018), which is confirmed to benefit signal propagation between neurons even when synapse coupling is suppressed or inactive. Therefore, researchers can build more neural circuits and explore signal encoding and transmission by capacitor and inductor coupling between hyperchaotic circuits. In an experimental method, Ren et al. (2019) confirmed that the synchronization between two Colpitts systems can be realized by building a transformer and

that the coupling coefficient of the transformer is an important bifurcation parameter for the synchronization manifold of the system. When field coupling is applied, secure communication can be further investigated using chaos synchronization. The coupling inductor and capacitor can also be used to collect external field energy; for example, electromagnetic radiation energy can be collected by these electric coupling devices and the coupled circuits will be regulated via energy flow.

In fact, we just discussed the case between two nonlinear circuits. The same further investigation becomes attractive and important when field coupling is considered between neurons in a network. As is well known, noise, time delay, and Calcium signal (Tang et al., 2017; Yu et al., 2017) can change the neural activities of neurons. Therefore, neural circuits can be connected via field coupling, and the collective behaviors can be detected for analysis of consensus and synchronization.

## 4 Conclusions

Based on chaotic PR circuits, symmetric coupling and cross coupling via a single variable are applied to investigate synchronization stability. It was found that symmetric coupling can support the stability of complete synchronization, while cross coupling, for which different channel variables were coupled, just triggers phase synchronization. When a linear resistor is used to activate voltage coupling, complete synchronization is reached while the coupling resistor has to consume a great deal of Joule heat and energy. Complete synchronization failed although phase synchronization can be stabilized when coupling is activated between the outputs from parasitic capacitance  $C_1$ , which holds a small capacitance. Complete synchronization, phase synchronization, and anti-phase synchronization can reach the desired target when capacitor coupling is activated, which can build a time-varying electric field, and the energy flow across the coupling capacitor is transmitted to further regulate the outputs and dynamics in the coupled circuits. In summary, capacitor coupling enhances the exchange of energy flow between the coupled circuits; as a result, the synchronization becomes relaxed and no additive energy is consumed as the coupling resistor.

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